

Offshore Wind Farm

Groundwater Risk Assessment and Monitoring Plan - Private Water Supplies and Licenced Abstractions (Part 4 of 4)

Document Reference: 9.66

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Revision: 0



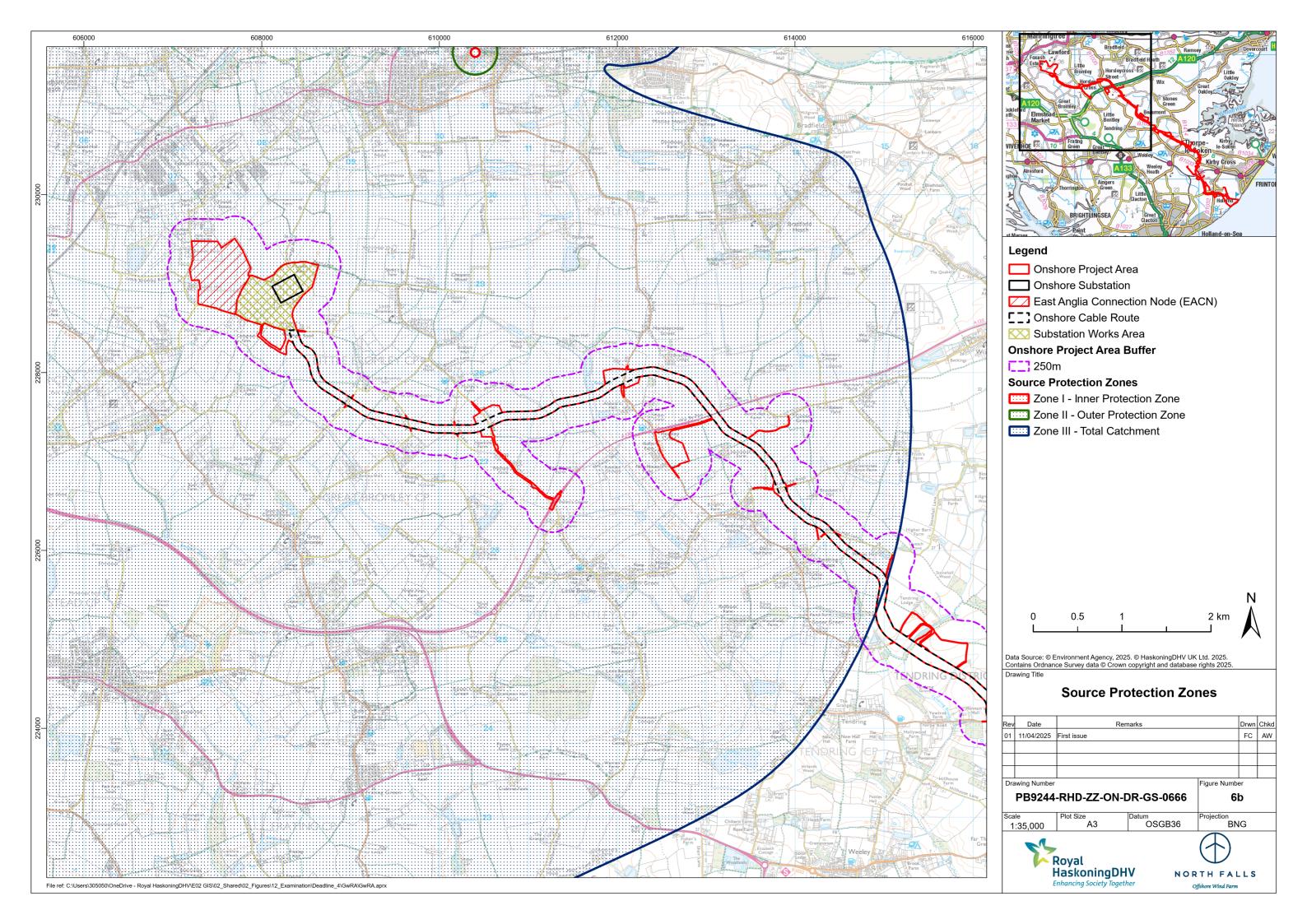


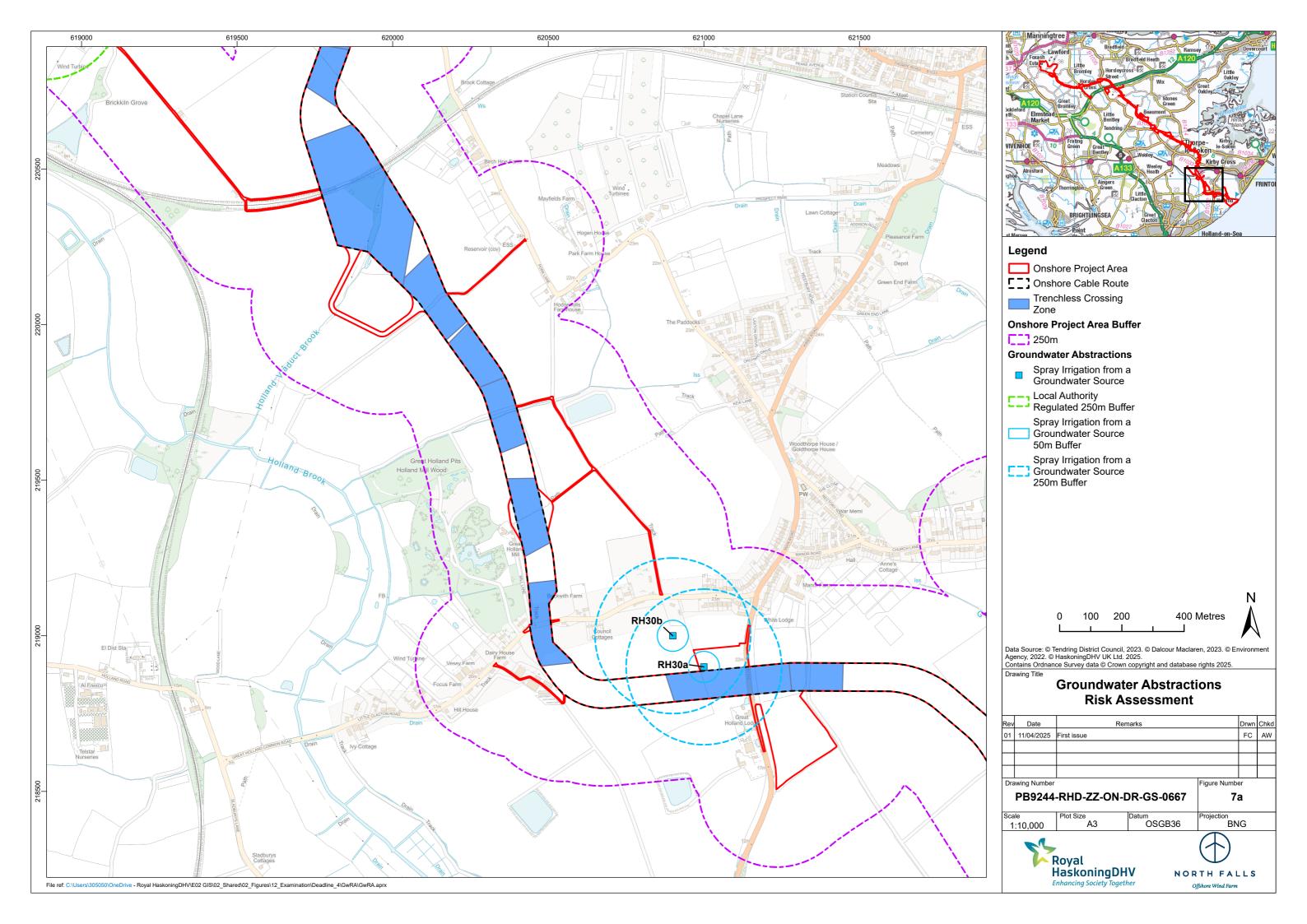
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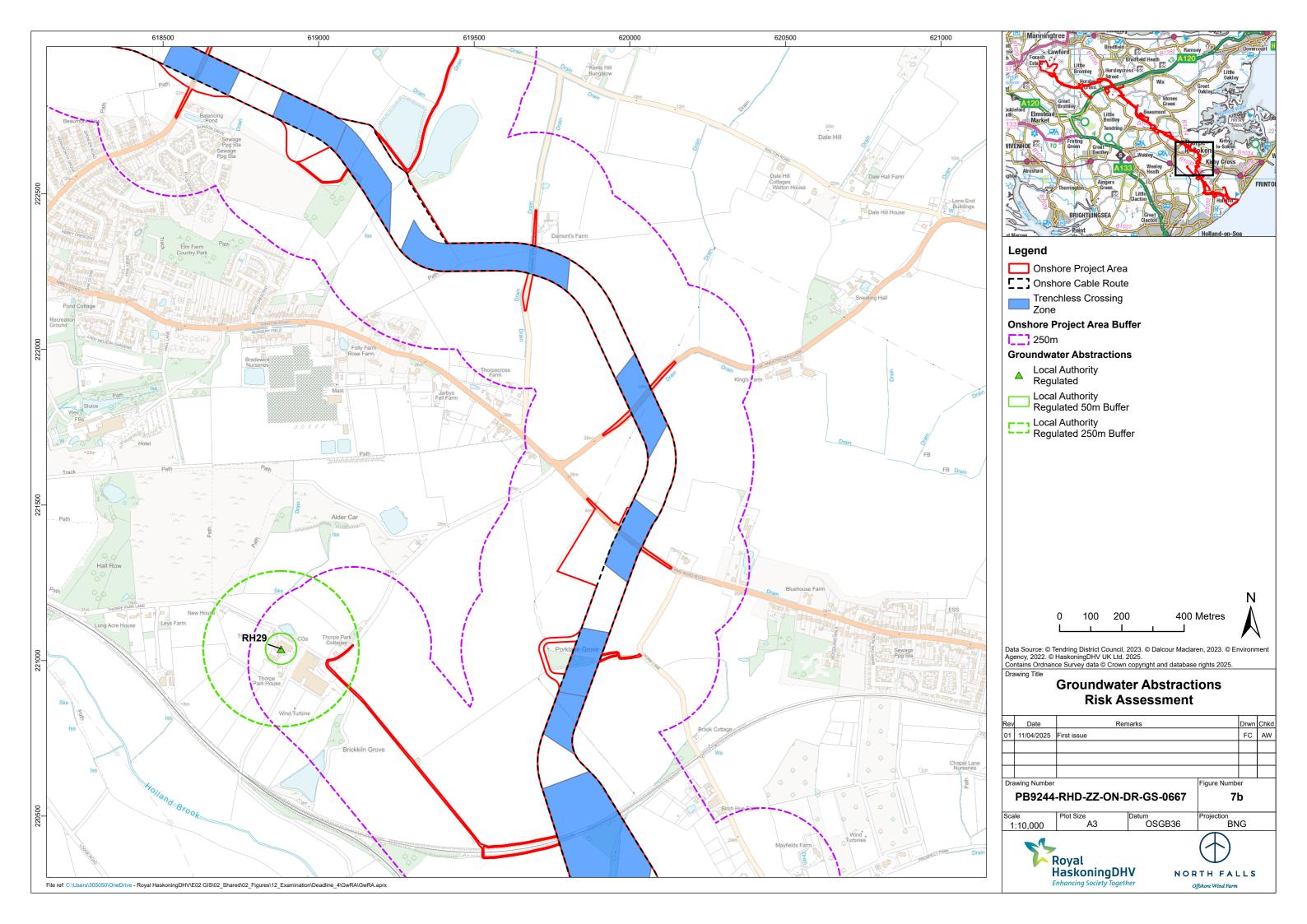
Project	North Falls Offshore Wind Farm
Document Title	Groundwater Risk Assessment and Monitoring Plan - Private Water Supplies and Licenced Abstractions (Part 4 of 4)
Document Reference	9.66
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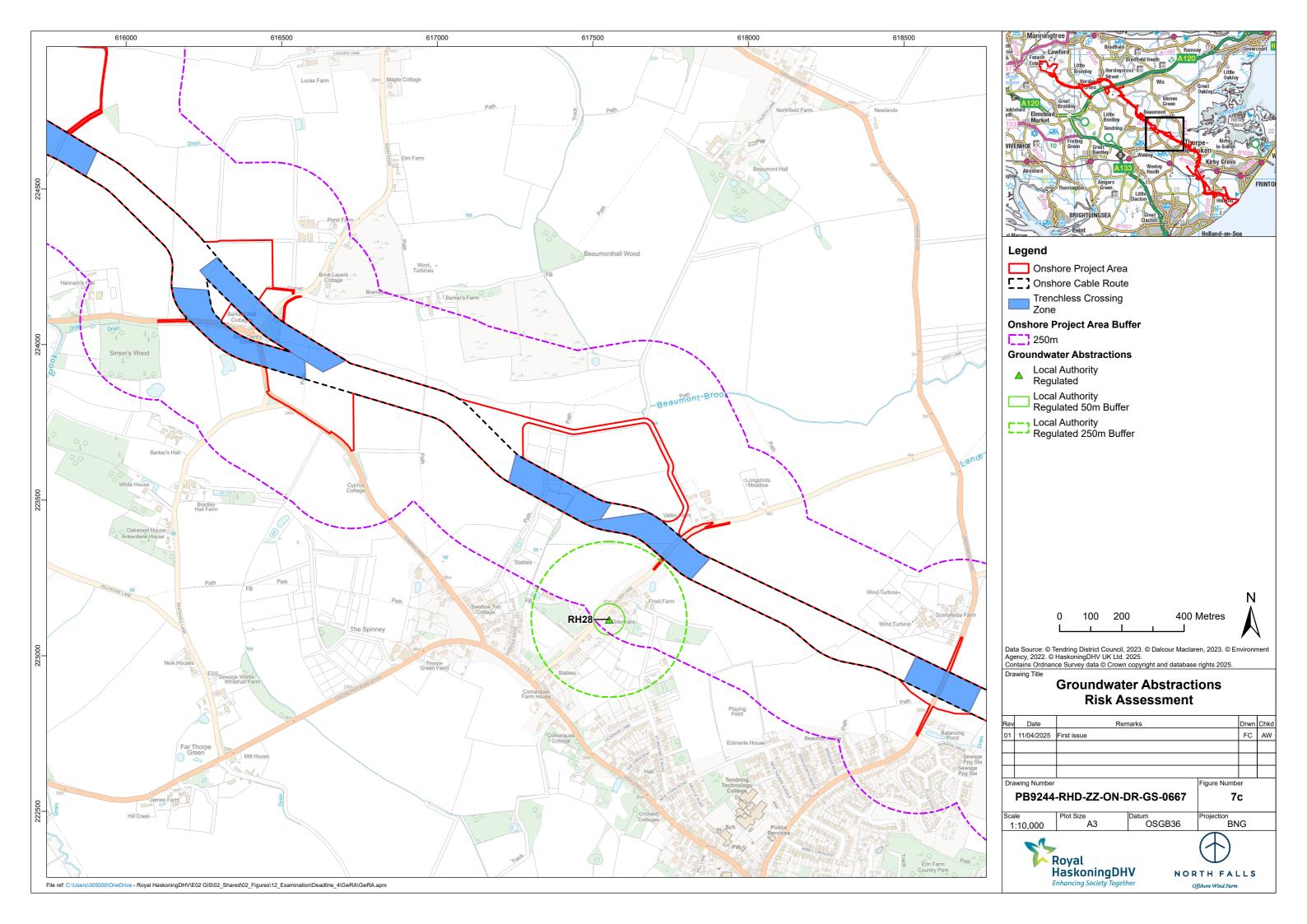
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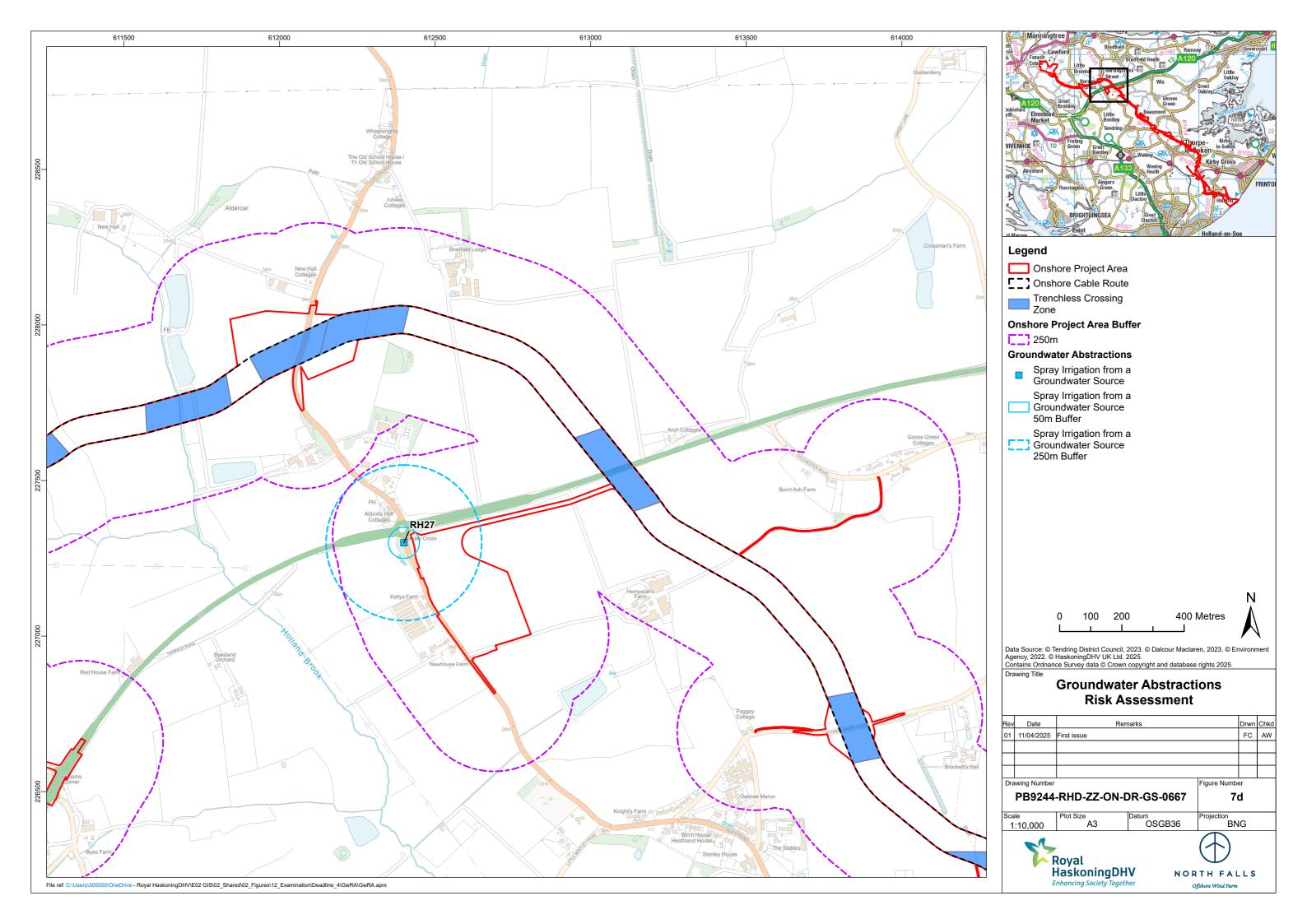
Revision	Date	Status/Reason for Issue	Originator	Checked	Approved
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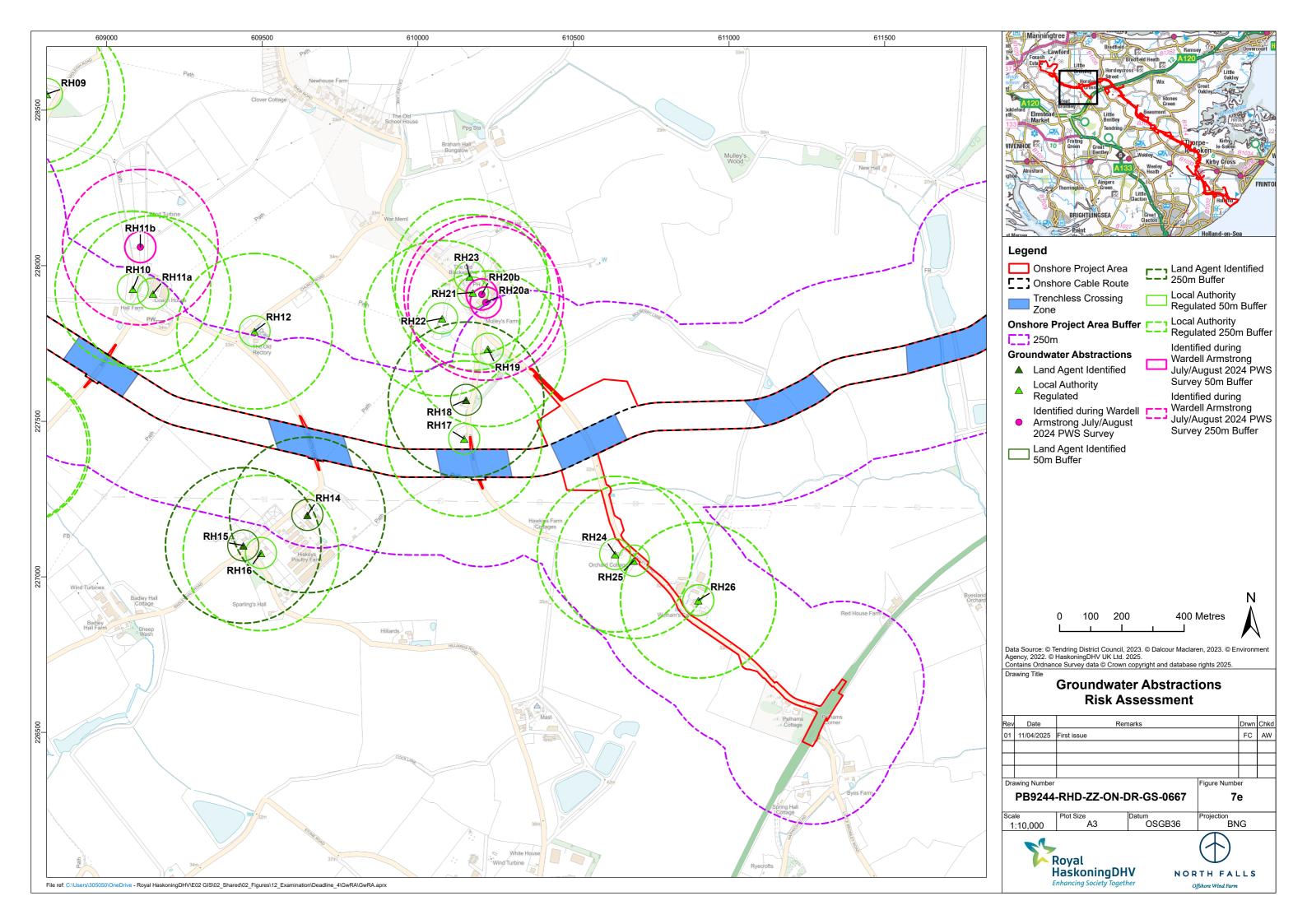


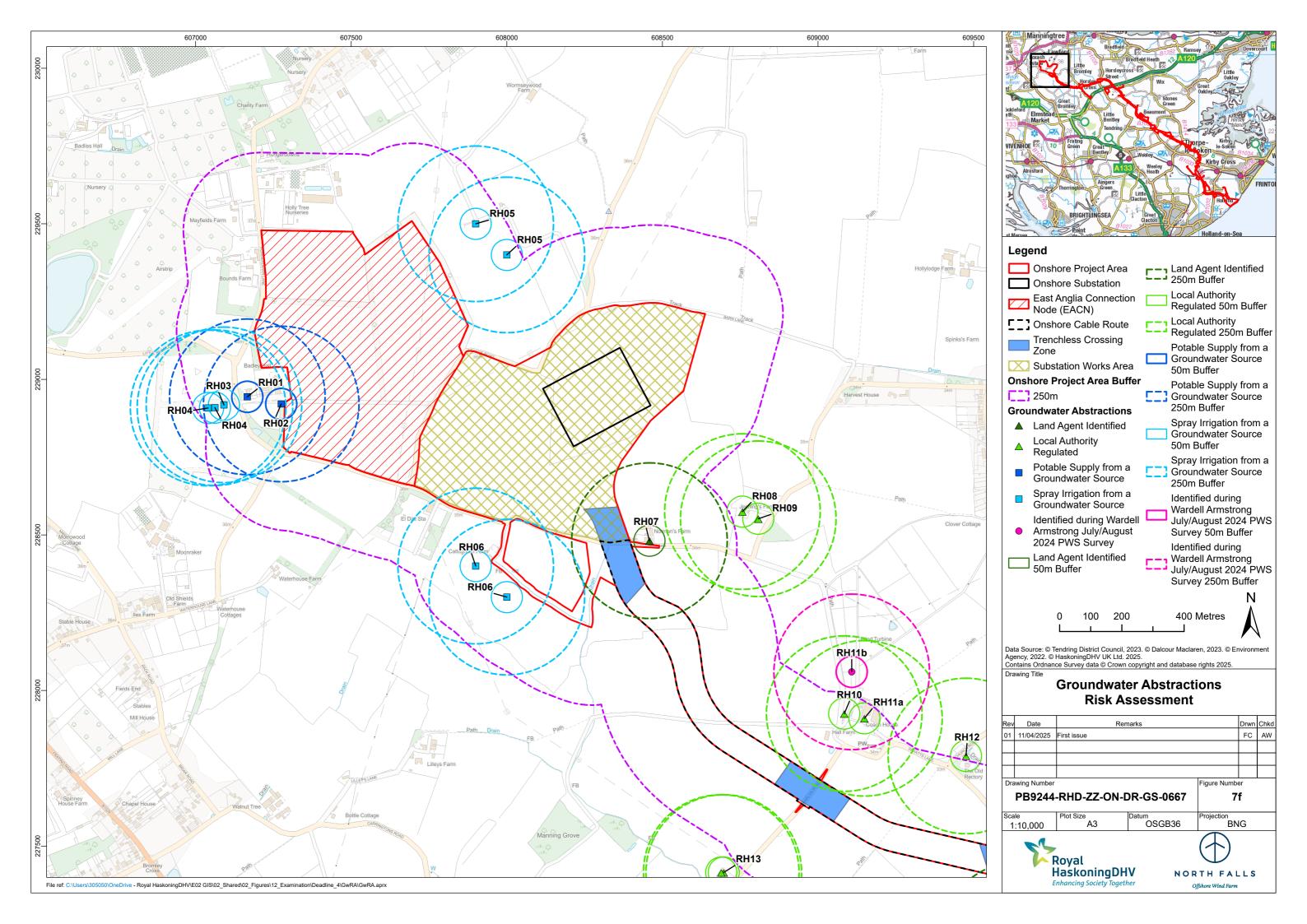


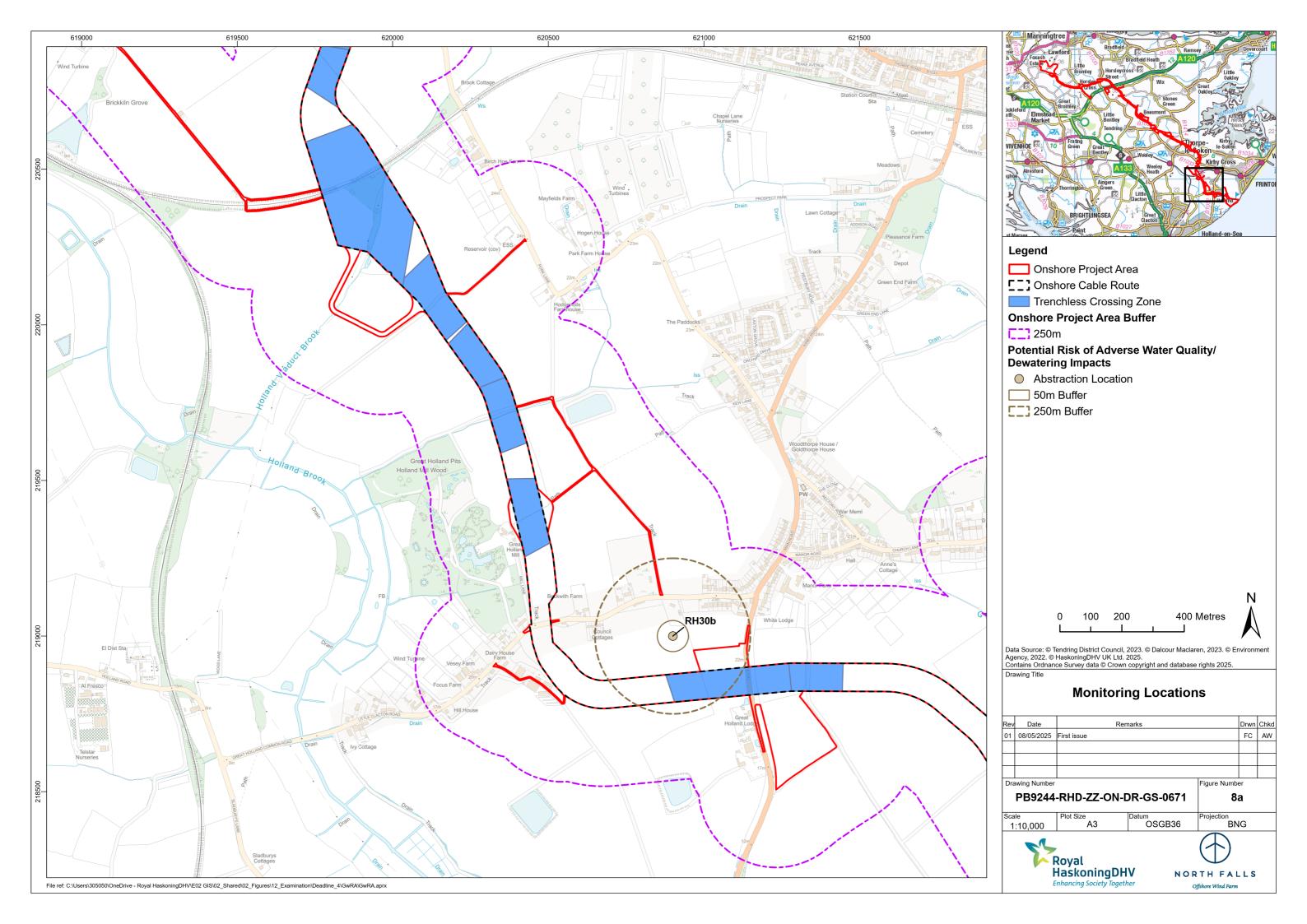


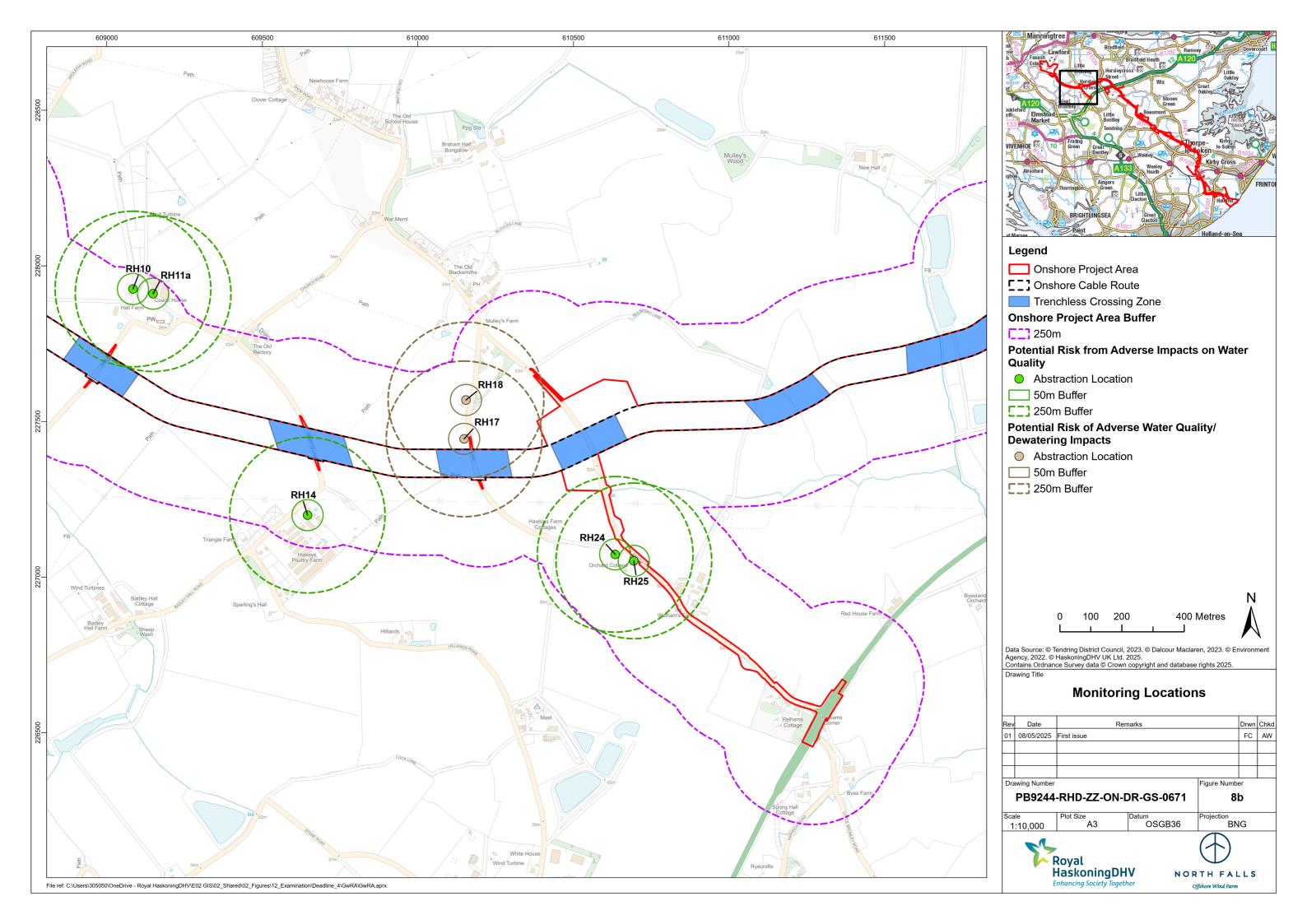


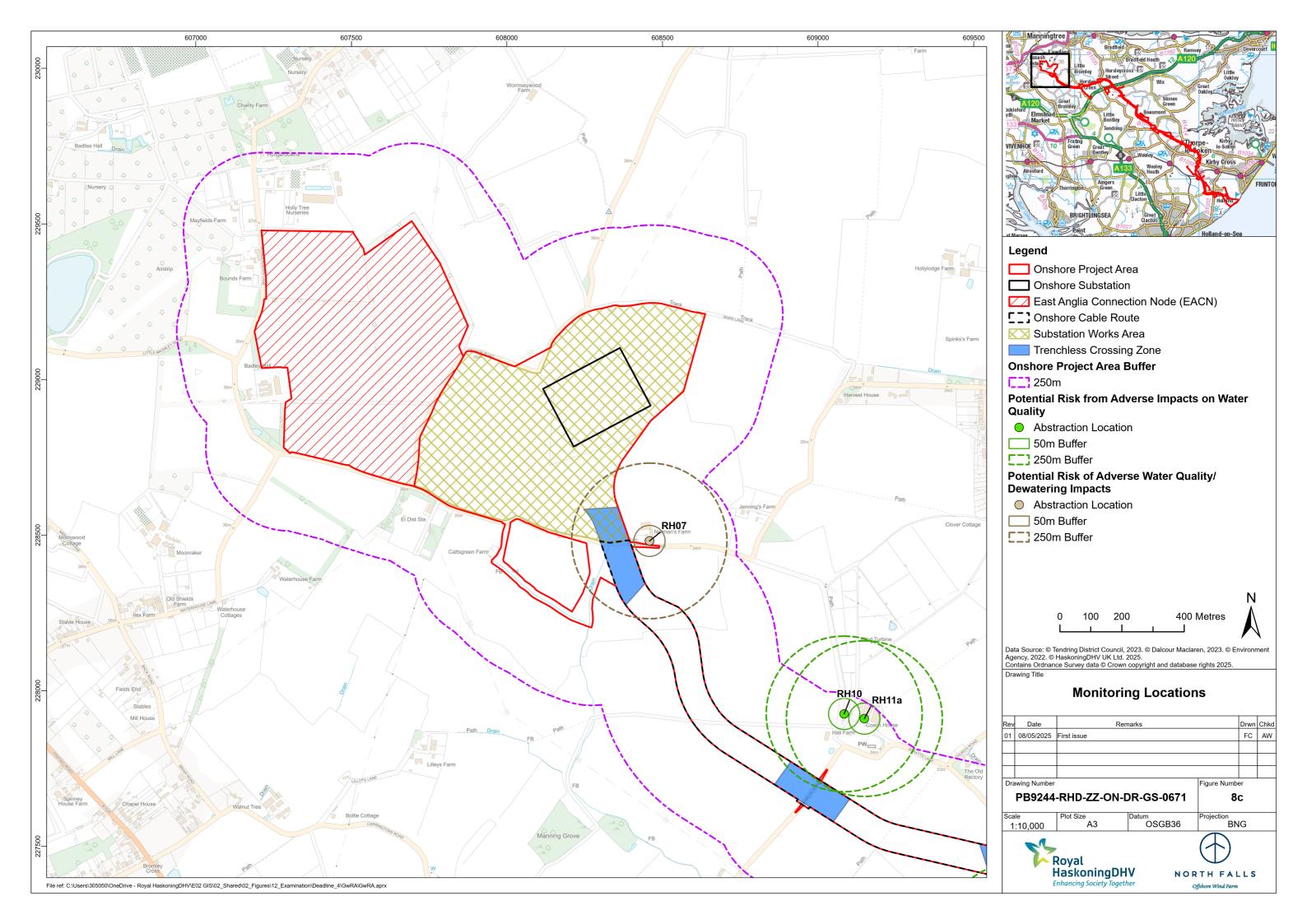












Appendix A. Report Limitations

Limitations

This report has been prepared by Royal HaskoningDHV with reasonable skill and care, within the terms of the contract with NFOW. The direct assessments and judgements given in this report are limited by both the finite data on which they are based and the proposed works to which they are addressed. The report has utilised a variety of publicly available data sources therefore the study is limited by the age and limitations inherent in the data. The acquisition of data is also constrained by both physical and economic factors and by definition is subject to the limitations imposed by the methods of investigations employed. In this instance the data has been obtained from samples and tests from mechanically excavated trial pits which by their nature only provide information about small discrete volumes of soil. They cannot provide data on every section of the ground beneath the site but the data are taken to be spatially representative of the zones of material between exploratory hole locations.

Conditions at the site will change over time due to natural variations and may be affected by human activities. In particular, groundwater, surface water and soil gas conditions should be anticipated to change with diurnal, seasonal and meteorological variations. Soil and water chemistry may change due to the actions of groundwater flows and microbiological activity etc. The likely variations in the data with time can be assessed following extended periods of measurement and statistical analyses. Unless specifically discussed in the text such extended measurement and analysis have not been carried out and the data collected are taken to be representative.

Appendix B. Borehole Summary

Table 1.1 Details of boreholes showing pertinent information within 100m of the Onshore Project Area

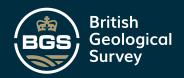
Borehole reference and Location	Details	Thicknesses
Landfall		
BH203 Maximum depth: 22.45mbgl (-21.54mOD) Centred on grid reference: 622684 218040	Topsoil: maximum depth: 0.10mbgl (0.81mOD) Alluvium (including peat): maximum depth 9.50mbgl (-8.59mOD) Possible Alluvium: maximum depth 11.20mbgl (-10.29mOD) London Clay Formation: maximum depth 22.45mbgl (-21.54mOD)	Topsoil:0.10m Possible/ Alluvium: 11.10m London Clay Formation:>11.25m
BH202 Maximum depth: 19.50mbgl (-18.36mOD) Centred on grid reference:622611 218103	Topsoil: maximum depth: 0.20mbgl (0.94mOD) Made ground: maximum depth 1.70mbgl (-0.56mOD) Alluvium (including peat): maximum depth 7.50mbgl (-6.36mOD) London Clay Formation: maximum depth 19.50mbgl (-18.36mOD)	Topsoil:0.20m Made Ground:0.30m Alluvium:4.80m London Clay Formation:>12.00m
BH201A Maximum depth: 20.20 mbgl (-19.23mOD) Centred on grid reference: 622509 218181	Alluvium: maximum depth: 7.20 mbgl (-6.23mOD) London Clay Formation: maximum depth 20.20 (-19.23mOD)	Alluvium:7.20m London Clay Formation:>13.00m
ECC		
BHLC-3 Maximum depth: 20.00mbgl (4.93mOD) Centred on grid reference:620659 219066	Topsoil: maximum depth: 0.20mbgl (24.73mOD) Possible Head: maximum depth 1.20mbgl (23.03mOD) Possible/ Cover Sands: maximum depth 5.60mbgl (19.33mOD) London Clay Formation: maximum depth 20.00mbgl (4.93mOD)	Topsoil:0.20m Possible Head:1.00m Possible/ Cover Sands:4.40m London Clay Formation:>14.40m
BHLC-1 Maximum depth: 20.00mbgl (3.40mOD) Centred on grid reference:620464 218963	Made ground: maximum depth: 2.00mbgl (21.40mOD) Kesgrave Catchment Subgroup: maximum depth 4.50mbgl (18.20mOD) London Clay Formation: maximum depth 20.00mbgl (3.40mOD)	Made Ground: 2.00m Kesgrave Catchment Subgroup:2.50m London Clay Formation:>15.50m
TM22SW14 and TM22SW18 to 21	Topsoil: Max depth 0.45mbgl	Topsoil:0.45m

Borehole reference and Location	Details	Thicknesses
Maximum depth: 12.19mbgl (mOD unknown)	Sandy Clay (Cover Sand?): Max depth 0.91mbgl	Possible Cover Sand:0.46m
Centred on grid reference: 620310 220230	Sand and Gravel (Kesgrave Catchment Subgroup?): Max depth: 3.66mbgl	Possible Kesgrave Catchment Subgroup:3.20m
	Stiff fissured Clay (London Clay Formation?): Max depth 12.19mbgl	Possible London Clay Formation:>8.53
BHR-S	Topsoil: maximum depth: 0.50mbgl (15.16mOD)	Topsoil:0.50m
Maximum depth: 25.45mbgl (-9.79mOD)	Possible Head: maximum depth 4.50mbgl (11.16mOD)	Possible Head:4.00m
Centred on grid reference: 619909 220374	London Clay Formation: maximum depth 25.45mbgl (-9.79mOD)	London Clay Formation:>20.95m
BHR-N	Topsoil: maximum depth: 0.30mbgl (22.68mOD)	Topsoil:0.30m
Maximum depth: 25.00mbgl (-2.02mOD)	Possible Head: maximum depth 0.50mbgl (22.48mOD)	Possible Head:0.20m
Centred on grid reference: 619734 220458	Possible Cover Sands: maximum depth 3.20mbgl (19.77mOD)	Possible Cover Sands:2.70m
	London Clay Formation: maximum depth 25.00mbgl (-2.02mOD)	London Clay Formation:>21.80m
BHSR-4	Made ground: maximum depth: 2.00mbgl (25.22mOD)	Made Ground: 2.00m
Maximum depth: 20.00mbgl (7.22mOD) Centred on grid reference: 616454 223967	Kesgrave Catchment Subgroup: maximum depth 2.90mbgl (24.32mOD)	Kesgrave Catchment Subgroup:0.90m
, and the second	London Clay Formation: maximum depth 20.00mbgl (7.22mOD)	London Clay Formation:>17.10m
BHSR-3	Topsoil: maximum depth: 0.20mbgl (26.42mOD)	Topsoil:0.20m
Maximum depth: 20.00mbgl (4.93mOD)	Possible/ Cover Sands: maximum depth 4.10mbgl (22.52mOD)	Possible Cover Sands:3.90m
Centred on grid reference: 616440 224087	London Clay Formation: maximum depth 20.00mbgl (4.93mOD)	London Clay Formation:>15.90m
BHSR-1	Topsoil: maximum depth: 0.30mbgl (21.03mOD)	Topsoil:0.30m
Maximum depth: 20.00mbgl (1.33mOD)	Made Ground maximum depth: 2.40mbgl (18.93mOD)	Made Ground:2.10m
Centred on grid reference: 616209 224098	London Clay Formation: maximum depth 20.00mbgl (6.62mOD)	London Clay Formation:>17.6m
TM12NW54	Possible Cover Sand (Sand and Gravel): maximum depth:15.24m	Possible Cover Sands:15.24m
Maximum depth: 20.11mbgl (mOD unknown)	London Clay Formation: Max depth 20.11mbgl.	London Clay Formation:>4.87m
Centred on grid reference: 613050 227500		

Borehole reference and Location	Details	Thicknesses
OnSS		
TM02NE15	Cover Sand: maximum depth: 2.70mbgl (31.70mOD)	Cover Sands:2.70m
Maximum depth: 10.10mbgl (24.3mOD)	Glacial Sandy Gravel: maximum depth 9.10mbgl (25.30mOD)	Glacial Sandy Gravel:3.40m
Centred on grid reference: 608430 22855	London Clay Formation: maximum depth 10.10mbgl (24.3mOD)	London Clay Formation:>1.00m
TM02NE14/A	Topsoil/ Made Ground: maximum depth 0.70mbgl (34.70mOD)	Topsoil/ Made Ground:0.70m
Maximum depth: 17.37mbgl (18.03mOD)	Cover Sands: maximum depth 11.89mbgl (23.51mOD)	Cover Sands:11.20m
Centred on grid reference: 608360 229220	Glacial Sand and Gravel: maximum depth 16.46mbgl (18.94mOD)	Glacial Sand and Gravel:4.57m
	London Clay Formation: maximum depth 17.37mbgl (18.03mOD)	London Clay Formation:>0.90m
TM02NE9	Topsoil and Made Ground: Max depth 1.10mbgl (34.90mOD)	Topsoil and Made Ground:1.10m
Maximum depth: 9.09mbgl (26.10mOD)	Glacial Sand and Gravel: 9.10mbgl (26.90mOD)	Glacial Sand and Gravel:8.00m
Centred on grid reference: 607250 228790	London Clay Formation: Max depth: 9.90mbgl (26.10mOD)	London Clay Formation:>0.80m

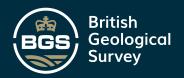
Note: All boreholes terminate in the London Clay Formation and therefore the strata thickness is likely an underestimate.

Appendix C. BGS Borehole Logs



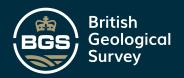
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Location Great Holland						u Levei.			
Client Tendering Hundred							<u></u>	<u> </u>	
\	RO	REHO							
STRATA	Legend	Depth below Ground Level		Type of Sample	tb/sq.ft.	deg.	m.c %	y lb/cu.ft.	N
Top Soil		1'0"	1'0"	-				-	
	- 1=	-		3'6"					
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					(CO			
				8' <u>6</u> "	13				24
Medium to Coarse Sand				1 1					24
and Gravel			18'0'					•	
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				13'5"	1				
				lT					12
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		100	1						
				18'6"	·				
				T					13
End of Boring		20'0"		1					
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(BCS)					(<	205)			
		(Bag							
Water Struck at 310"			Ma	ximum C	Dbserved \	Water Le	evel 2	1611 -	



TM 22 SW 12

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	SITE	ST & INVESTIGNEW Y	ATION ORK	DEPT.	. (,				
Contract No. 19495/B697		LEED)S, 2		Borebo	ole No		1	
Location Great Holland W	ater To	ower							
Client Tendering Hundr				•••		May			
Cilette		REHO		LOG					
STRATA	Legend	Depth below Ground Level	Thickness of Strata	Type of Sample	c lb/sq. ft.	ø deg.	m.c %	y lb/cu. ft.	N
Top Soil		113"	1'3"					-	
Stiff Orange Brown Very Sandy Clay	- -	3'6"	213"	3'6" T					24
Sand and Gravel				8 '6"	(;	205)			29
		(80	20'6'	13'6" I 18'6"					10
		24'0"		20'0"	1900	0	34	118	
Stiff Fissured Grey Clay			15'6	28'6"	1400	0	35	117	
		(BC		33'6"	2300	0	34	118	(0)
End of Boring		40'0"		38'0"	2600	0	31	122	
Water Struck at - 4 0"			Ma	ximum O	bserved \	Water Le	vel -	 3'	0"



TM \$2 NW/Ba-e 1375.2646 1342.2653

Heath Hospital, Tendring 224/88

(a) (Filled in). Surface +116. Shaft 106%; rest bore. Lining tubes: 68 x 8% in 1352-2635

from 94% down (perforated 140% to 160%). Ck -103%. R.W.L. +25. LeGrand, 1903.

(b) (? Filled in). Surface +c.110. Bore 340. Lining tubes: 16% × 8 in; 120 × 6 in. | Ck -2.24, | Ck -c.106. R.W.L. -c.2. Yield 300 g.p.h. Saline. Richards, 1925.

(a)	Sand and Gravel) LC)	•••	•••	160%	160%
	WRB	•••		59	219%
	UCk	•••		2801/4	500

(a)

		THIC	KNESS	DEP	TH
or Survey use only). GEOLOGICAL LASSIFICATION.	NATURE OF STRATA (and any additional remarks).	Feet.	Inches.	Feet.	Inches
Only	Dug well			106	6
Orgin Um	Rublick			107	6
10	Blue clay	42		149	6
Woolinich t	Pebbles, sand water	5		160	6
Region	mottled clay	17	6	178	
59'	Hard sandy clay	12		201	
	Dark green sondy clay	8	6	209	6
. p. sarra consensation to a consequent	Chalk a Philo	10 108		327	6
Jepa de.	Sticky chalk	3		330	- 5
Ch 2801	Soft study clack	10		340	
	Sich chell a few flits	/45	6	500	

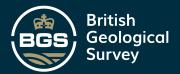
88 (67

Drift 16 (C)

Drift 16 d)

Drift 16 PP LPT 11/1/69.

For details g (b), (c), (d), (e) see Additional Information sheet



→ 224/88 Heath Hospital, Tendring

TM 12/16 A4B

(a) (Filled in). Surface +116. Shaft 106%; rest bore. Lining tubes: 68 × 8% in from 94% down (perforated 140% to 160%). Ck -103%. R.W.L. +25. LeGrand. 1903.

(b) (? Filled in). Surface +c.110. Bore 340. Lining tubes: 16% × 8 in; 120 × 6

(b) (? Filled in). Surface +c.110. Bore 340. Lining tubes: 16% × 8 in; 120 × 6 in. Ck' -c.106. R.W.L. -c.2. Yield 300 g.p.h. Saline. Richards, 1925.

				•	
(a) (b) (c) 7	nd and Gravel)	•••	•••	160%	160%
, WRI	3	•••	•••	59	219%
/ va	C	• • *•	•••	280%	500

404

or Survey use only).	NATURE OF STRATA	THIC	KNESS	DEF	TH
GEOLOGICAL LASSIFICATION.	(and any additional remarks).	Feet.	Inches.	Feet.	Inches
Originalian Clay	Oug well			106	6
(mon (m)	Rublish			167	6
_14	Blue slay Pebbles, sand water	42		149	6
Working 1	Longlamesate	5	6	160	6
1800	mottled clay sandy	12		190	
59 7	Hard sandy clay			201	
	" fard "	10	6	327	6
الموصوبي.	Chalk of flicts Sticky chalk	/08 3	-	336	6
Chor 286%	Chall mark Soft stick stack	10		340 354	
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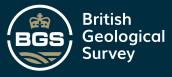
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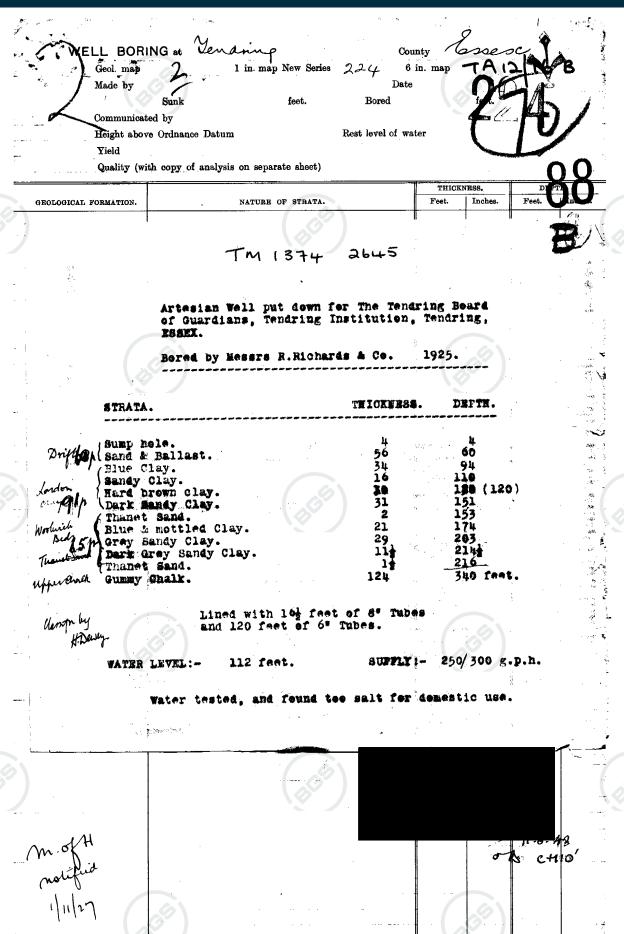
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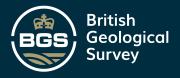
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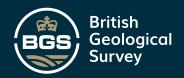
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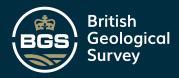
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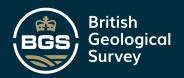
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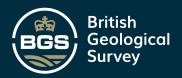


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	(BCS)			



· Salaki.

TM DA NE /15

TM 02 NE 15

0843,2855

Opposite Rudkin's Farm

Block C

Surface level (+34.4 m) +113 ft* Water struck at (+31.7 m) +104 ft Wirth B0, 8 inch diameter November 1969

Overburden (2.7 m) 9 ft Mineral (6.4 m) 21 ft Bedrock (0.9 m+) 3 ft+

Glacial Sand and Gravel

Sandy gravel. Very sandy near top and gravelly between 24 ft (7.3 m) and 27 ft (8.2 m).

Gravel: fine subangular flint and quartz, with coarse, subangular to subrounded flint the latter approaching cobble size between 24 ft (7.3 m) and 27 ft (8.2 m), where coarse gravel is predominant.

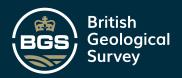
Sand: reddish-brown; medium, with some coarse.

Thickness (m) ft	Depth (m)	ft
(2.7) 9	(2.7)	9
(6.4) 21	(9.1)	30
	. 4	
(0)		

London Clay Brown, weathered clay, passing down into fresh blue clay.

(0.9+) 3+ (10.1)

% mm		mm	%		Depth below	Percentages			
/0 111111	/0		surface (ft)		Fines	Sand	Gravel		
Gravel	40	+16	:	18	9 - 12		8	75	17
		-16+4	:	22	12 - 15.		2	53	45
Sand	57	-4+1	•	12	15 - 18 18 - 21		0	67	33
		$-1+\frac{1}{4}$:	40	21 - 24		0	57	39
		$-\frac{1}{4}+1/16$:	5	24 - 27	1	0 .	63 33	37 67
Fines	3	-1/16	:	3	27 - 30		4	58	38



TM 02 NE /14

Depth

(m).

0.7

IMAN Database NO TMOZNE 14RZ

TM 02 NE 14

0835 2922

Lower Barn

Block C

Surface level (+35.4 m) +116 ft Water struck at +32.6 m (+107 ft) Pilcon Shell, 6 inch diameter December 1970

Overburden 1.6 m (5 ft) Mineral 8.5 m (28 ft) Bedrock 0.5 m+ (1.5 ft+)

ft

(2.5)

Thickness

(m)

0.7

Topsoil and made ground.

Loam

Silty and clayey sand with some gravel.
Sand orange-brown in colour; mainly medium; rounded to subangular quartz.
Grave. composed of fine grade, rounded to subangular flint and quartz.

0.9 (3) 1.6 (5)

Glacial Sand and Gravel

Grave. composed of fine grade, rounded to sub ingular flint and quartz.

Sandy gravel. Gravelly down to 6.6 m

8.5 (28) 10.1 (33)

(21.5 f:), becoming very sandy below.

Grave:: mainly fine with some coarse and a few cobbles down to 6.6 m (21.5 ft), traces only of fine to coarse below; rounded, subrounded and subangular flint with subordinate quartz and quartzite.

Sand: medium with coarse to 6.6 m (21.5 ft), becoming fine with medium below: brown

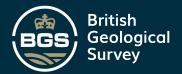
becoming fine with medium below; brown to orange-brown colour; thin, pale grey, clay band at about 8.5 m (28 ft).

London Clay

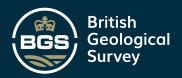
Blue-grey, stiff clay.

0.5+ (1.5+) 10.6

nt			Depth below	1 1	Percentages	. 1
% mm	mm	1 % .	surface (m)	Fine	s Sand	Gravel
Gravel 30	+64 :	1	1.6 - 2.6	'4	60	36
	-64+16 :	10	2.6 - 3.6	. 1	63	36
	-16+4 :	19	3.6 - 4.6	. 0	56	44
			4.6 - 5.6	1	37	62
1nd 68	-4+1:	10	5.6 - 6.6	2	54	44 .
	$-1+\frac{1}{4}$:	33	6.6 - 7.6	3	96	1
	$-\frac{1}{4}+1/16$:	25	7.6 - 8.6	1.	95	4
			8.6 - 9.6	2	76	22
ines 2	-1/16 :	2	9.6 - 10.1	2	93	5



	Mi Sa BC	neral A	Geologica Assessmen Gravel St RECORD SI	ırvey HEET	Summar	Nat. Gri Locality Date: & Recorded	d Ref	No.: TM :: 083° wer Bam, 20th May	5,29 Baml	22 ane		•
a ic drill lo	Drill Hole d	Type: iameter level struck	Widh 1 c: 8' (0.D.): at (0.D.)): 5'6s 2'6.s.	grou penetr	nd 1	İ	(Top Soil	Brown	on C	Jay	
	Remark <u>Gradir</u>	اكتط	Armell oct	he histe w that dep er the (b	Mean Gradin	re was i	25t4	Fines	Depth baile Sand	d: c	.5 feet Gravel	er 50 .
	hean Grading Perconteges, for the Assessed Minoral Phickness % by weight passing 0 20 40 60 80 100	Fines			percen 1 rticle s	4 size (nm)	Gré	avel 64	Depth in feet	10 - 20 - 30 - 40 - 50 - 60 - 70 - 80 -		Diagram to show varietion in the pro- portion of Fines, Sand and Gravel with Depth
,	Top Soil Brown	l	9)	on of Stra		of chall	٤,	Depth to base ft.	Thickr ft. I-O 4-C		Sample Nos.	
	Brown Clay - soft day; Sand Sand with Gravel: Sand: med to co; brown Gravel: fine to med: A-S.F. with RS.A. qua L.P.S. 30 mm. Gravel percent aga increases up					ng S.A. qu (black + l	љ. moush),	20 0	15.0		CH 14 CH 14 CH 14 CH 14	-03 -02
	Sound	and	Iravel	?? d due				25.0+	5.1	5	No Re	COVERY



TM OR NE 19

	10							
TM ()2 NE 9	072	25 2879	Near B	adley Hall		BI	ock C
Wate Shell	ice level (+36, r struck at +3 and Auger, 6 mber 1970	.0 m) +118 ft 32.0 m (+105 f 5 inch diamete	r		Minera Waste Minera	rden 1.1 ; 1 3.4 m (3.2 m (10. 1 1.4 m (4 k 0.8 m+	11 ft) 5 ft) .5 ft)	
			(BE	2)	Thicknown m	ess (ft)	Depth m	(ft)
Tops	oil and made g	ground.			1.1	(3.5)	1.1	(3.5)
	al Sand (a) Fravel	, roui.ded roui ded	nainly fine; suba brown and red fli quartzites.	nts, with	3.4	(11)	4.5	(15)
	(BC	Yellow-brow becoming material,	vn, laminated, siblue-grey with ca and then dark bro flints and quartz	ilty sand, rbonaceous own with	3.2 m	(10.5)	7. 7	(25.5)
	(b)	gravelly do Gravel: fir to rounded; jasper pebl Sand: med	ne with some coa flints and quart	rse; subroundersite with a few	v	(4.5,)	9.1	(30)
Londo	n Clay	Blue clay, w (2 ft).	eathered brown i	n top 0.6 m	0.8+	(2.5+)	9.9	(32.5)
Mean	(a) + (b)		•		1		٠	
Gravel		%: 13 (a)	Depth below surface (ft) 1.1 - 2.1	:		centages Sand C	Gravel	
Sand	$ \begin{array}{rrr} -16+4 \\ 57 & -4+1 \\ -1+\frac{1}{4} \\ -\frac{1}{4}+1/16 \end{array} $: 28 : 19 : 33 : 5	2.1 - 3.1 3.1 - 4.1 4.1 - 4.5 Mean	1	1 2 2 2 2	67 56 65 59	32 42 33 39	
Fines	2 -1/16	(b)	7.7 - 8.7 8.7 - 9.1 Mean	1	2 1 2	53 49 52	45 50 46	

Appendix D. Outline Groundwater Monitoring and Mitigation Plan

D.1 Background

1. Based on the findings of the Groundwater Risk Assessment (GwRA) for the North Falls Offshore Wind Farm ('North Falls' or 'the Project') including the proposed landfall, onshore cable route and onshore substation works area a groundwater monitoring and mitigation plan (GwMP) is recommended to ensure that there are no adverse impacts from the construction phase on surrounding private water supplies (PWS) and the licenced abstraction.

D.2 Summary

- 2. Locations have been identified whereby either one or a combination of surveys / assessments are required including:
 - Topographical survey.
 - Baseline data collection to include groundwater level monitoring, a landowner discussion and an assessment of the abstraction.
 - Extended groundwater level monitoring
 - Water quality monitoring.
- 3. These recommendations are summarised in Table D1.

Table D1 Summary of Locations Whereby Further Work and Monitoring is Recommended

RH Location ID	Location Address	National Grid Reference	Distance from Potential Onshore Cable Route Dewatering Activities (direction) or feature that has	Topogra phical Survey	Initial baseline Monitoring	Extended Groundwater Level	Water Quality Monitoring and routine groundwater levels obtained during sampling	
	triggered further assessment Abstraction type and feature Assessment Visit Required		Assessment Visit	Monitoring Due to the Risk of Dewatering Activities	Extended Groundwater Monitoring Suite Table D2	Reduced Groundwater Monitoring Suite Table D3		
RH07	Normans Farm	608458E 228481N	10m (north) Construction / Access Road and 60m (east) from Onshore Cable Corridor / TCZ	✓	N/A	✓	√	N/A
RH10	The Coach House	609084E 227925N	185m (northeast) from Access / Construction Road and 220m (northeast) from Onshore CC / TCZ	✓	N/A	N/A	N/A	✓
RH11a	Little Bromley Hall	609149E 227910N	205m (northeast) from Construction / Access Road and 245m (northeast) from Onshore CC / TCZ	✓	N/A	N/A	N/A	✓
RH14	Hiskleys Farm Kennels	609645E 227199N	150m (south) from Access / Construction Road and 180m (south) from Onshore CC / TCZ	✓	✓	N/A	N/A	✓
RH17	Paynes Cottage	610149E 227444N	20m (west) from the Construction / Access Road and 35m (north) from Onshore CC / TCZ	✓	N/A	✓	1	N/A
RH18	Richmond Cottage	610155E 227569N	120m (north) from the Construction / Access Road and	✓	✓	✓	N/A	✓

RH Location ID	Location Address	National Grid Reference	Distance from Potential Onshore Cable Route Dewatering Activities (direction) or feature that has triggered further assessment type and feature	e Route phical ctivities Survey feature that has ner assessment ure		Extended Groundwater Level Monitoring Due to the Risk of Dewatering Activities	Water Quality Management of the continuous c	water levels
			160m (north) from Onshore CC / TCZ					
RH24	Oakwood	610634E 227073N	35m (southwest) from Construction / Access Road	✓	N/A	N/A	N/A	✓
RH25	Orchard Cottage	610694E 227052N	10m (southwest) from Construction / Access Road	✓	✓	N/A	N/A	✓
RH30b	A H Brown Farms Dairy House	620900E 219000N	80m (north) from the Construction / Access Road and 120m (north) from Onshore CC / TCZ	√	√	√	√	N/A

- 4. This outline GwMP will be updated and confirmed following finalised design, survey works, location of construction techniques, micrositing of the cable within the onshore cable route and confirmation of groundwater needs during the construction phase from the land owners. The final GwMP, produced in accordance with this outline, will be submitted for approval to the relevant authorities and secured through a DCO requirement.
- 5. Monitoring will be completed from the PWS and the licenced abstraction outlined in Table D1, unless agreed with the landowner that monitoring is not required for instance if the abstraction(s) are no longer in use or if the actual surveyed location is further from the onshore project area than initially thought. Locations are presented on Figure 8.

D.3 Surveying, Monitoring and Sampling Plan

6. This section summarises how data gaps are to be filled, what baseline data is required and outlines details of each element of monitoring set out in Table D1.

D.3.1 Topographical Survey

7. All of the locations listed in Table D1 require a topographical survey to confirm the coordinates of the abstraction supply and the ground level of the abstraction so groundwater level can be adequately assessed in relation to its proximity and elevation in comparison with the onshore project area.

D.3.2 Baseline Data Collection to Include Groundwater Level Monitoring, A Landowner Discussion and an Assessment of the Abstraction

8. There are locations where the baseline groundwater level survey has not been completed or the source of information is uncertain, including RH14, RH18, RH25 and RH30b.Information pertaining to treatment and details around the abstraction i.e. depth, type, casing type, size etc needs to be completed.

D.3.3 Groundwater level monitoring

9. For the PWS and the licenced abstraction which could potentially be impacted by the dewatering activities and adverse groundwater quality along the onshore cable route, including RH07, RH17, RH18 and RH30b, new boreholes could potentially be sunk into the shallow superficial deposits and installed with continuous shallow groundwater level logger monitoring equipment. If this option is undertaken, these should be located between the abstraction and the onshore cable route subject to landowner agreement. This first line of defence should identify an issue prior to impacting the abstraction point. The level logger data should be collected a month before the dewatering activities start, during and post dewatering activities finishing. This is to allow for natural variations to be monitored that may occur in the groundwater table due to other external factors such as dry spells or heavy rain. A barometric logger must be installed to allow for compensation due to atmospheric pressures.

- 10.It may be deemed appropriate to install a level logger within the actual abstraction, however, this would be subject to agreement with the landowner / tenant.
- 11. In order to monitor in real time, a telemetry system could be considered to be used, so impact of the dewatering can be assessed in real time.
- 12.PWS beyond the risk of being impacted by dewatering but may be subject to water quality impacts, monitoring will require groundwater level monitoring to be undertaken routinely when the samples are obtained for laboratory testing.

D.3.4 Water Quality Requirements

- 13. The following outline water quality monitoring plan is based on the findings of the PWS and the licenced abstraction assessment and water quality testing requirements for private water supplies as outlined within The Private Water Supplies (England) Regulations 2016 (as amended) (Regulations) and will be completed throughout the proposed construction phase. There are two monitoring suites proposed:
 - Suite 1: PWS and the licenced abstraction within 100m of dewatering activities will be monitored for all parameters outlined in Part I and Part II of Schedule 1 of the Regulations. In addition, groundwater level monitoring will be undertaken.
 - Suite 2: PWS in excess of 100m from dewatering activities but in close proximity to construction activity which have the potential to impact water quality will be monitored for a reduced suite, as outlined by Part II of Schedule 1 of the Regulations. In addition, groundwater level monitoring will be undertaken.

D.3.5 Monitoring Methodology and Procedure

- 14. To confirm the requirement for monitoring at each PWS and the licenced abstraction listed in Table D1 a licenced abstraction agreement will be made with the landowner / tenant prior to the construction works along the onshore cable route. If there is no requirement for the groundwater supply during the construction phase (i.e. due to the availability of alternate supply or lack of need), the pre-commencement and post-development confirmatory monitoring only will be required. If a groundwater supply is required during construction, there will be a requirement for the required monitoring suite to be tested for summarised in Table D2 and D3.
- 15. Monitoring would be undertaken prior to, during and after the construction phase at a timing a frequency summarised in Table D2 and D3.

D.4 Sample Collection Procedure

16. The sampling method used will be at the discretion of the contractor depending on the nature of the water supply. The groundwater sample should be taken

prior to any local treatment (i.e. from the well rather than the tap). Where the well has not been in regular use samples should be taken using the most appropriate equipment e.g. a pump or a bailer. Prior to the sampling the borehole should be purged using either a surface mounted or a submersible pump. Where possible, three well volumes should be purged to allow removal of stagnant water from the borehole and allow fresh water to be sampled. The well volume should be calculated using the following formula:

$$V = \frac{\pi}{4} \times (d)^2 \times (h - Static water depth)$$

 $V = Well \ volume \ (m^3)$

 π = 3.14159

d = Well diameter (m)

h = Total well depth (m)

Static water depth (m)

D.5 Sample Preparation, Preservation and Transport

17. In accordance with accredited laboratory best practice filtration should take place in the field for dissolved heavy metals using a 0.45µm in-line filter, in order to prevent precipitation of metal species during transportation. The filtered water should be placed in a 150ml plastic bottle containing nitric acid, however this will need to be confirmed with the chosen laboratory and what their accreditation requirements are. Additionally, Samples should be filled to the top of the bottle neck until a meniscus forms. This ensures that all air has been excluded from the samples, which helps to prevent oxidation of the sample. It can also prevent removal of other dissolved gases from solution. Samples should be delivered to the selected ISO/17025 accredited laboratory with the relevant chain of custody form completed within 24 hours of sampling.

D.6 Proposed Monitoring Schedule

18. The proposed monitoring schedule for PWS and the licenced abstraction at risk of dewatering impacts and groundwater quality impacts listed in Table D1 is detailed in D2 and D3 respectively.

Table D2 Extended Groundwater Level Monitoring and Laboratory Testing Schedule

RH Location ID	Monitoring Parameter	Frequency	Data collected	Further Information	
RH07 RH17 RH18 RH30b	Groundwater Level monitoring	Continuous using Level Loggers	Groundwater level (m bgl) to be corrected using the barometric logger.	To be undertaken during periods of dewatering with commencement 1 month prior of dewatering and continual monitoring until 1 month after the dewatering has stopped.	
	Field Measurements and Field Groundwater Level monitoring	Weekly	pH, oxidation redox potential, dissolved oxygen, electrical conductivity, resistivity, salinity, total dissolved solids and turbidity.	To be completed a month before, during and a month post dewatering.	
	Laboratory Measurements and Field Groundwater Level monitoring	Monthly	Wholesome Test: See Schedule 1: The Private Water Supply Regulations (England) 2016. Schedule 1 Part I and II.	Sampling to be undertaken three months before the dewatering works starts, monthly during and for three months after the dewatering has stopped.	

Table D3 Groundwater Level Monitoring and Reduced Laboratory Suite Water Quality Monitoring Schedule

RH Location ID	Monitoring Parameter	Frequency	Data collected	Further Information	
RH10	Groundwater Level monitoring		Groundwater level (m bgl) Depth to base of the well		
RH11a RH14 RH24	Measurements		pH, oxidation redox potential, dissolved oxygen, electrical conductivity, resistivity, salinity, total dissolved solids and turbidity.	Monitoring to start 1 month prior to the construction works, monthly during and monthly monitoring for a period of three months after the construction works has stopped.	
RH25	Laboratory Measurements		Reduced Suite: See Schedule 1 Part II: : The Private Water Supply Regulations (England) 2016.		

D.6.1 Data Keeping and Reporting

- 19. The following should be recorded during all relevant monitoring:
 - Date and time at which water level was recorded and accurate sample reference.
 - Sampling equipment, serial number and method.
 - Volume of groundwater purged, prior to sampling.
 - Response to pumping (pump rate, drawdown at end of pumping).
 - Observations of any potential contamination or movement including water colour, turbidity, odour.
 - Observations of damage to installations.
 - Name of sampling personnel.
 - Weather condition during the monitoring.

D.6.2 Data Format

20. Collected data from each monitoring visit should be inputted into a digital format e.g. Microsoft Excel.

D.6.3 Quality Control and Assurance

21. Monitoring and sampling should be undertaken by a suitably qualified engineer in accordance with the proposed monitoring procedures. Monitoring equipment and instrumentation should be serviced and maintained in accordance with the manufacturers' recommendations. Calibration records should be kept and filed accordingly. A suitably accredited laboratory should carry out analysis of groundwater samples which are to be tested for drinking water parameters.

D.7 Mitigation Planning

D.7.1 Water Quality

- 22. The data should be assessed against baseline data and relevant UK Drinking Water Standards (DWS), as outlined in The Water Supply (Water Quality) Regulations 2016 (as amended) to ensure no adverse impact on the PWS and the licenced abstraction. The water quality data should be reviewed following each monitoring round and in the event of an exceedance of DWS or the baseline data the following measures would be undertaken:
 - Request a re-test of the sample from the lab to ensure the result is correct.
 - Review the latest monitoring against the baseline water quality data collected prior to commencement of working to determine if the exceedance is consistent with baseline data.

- If the monitoring indicates a deterioration in water quality since baseline monitoring temporarily increased to weekly to allow for further review.
- Provide a provision for temporary alternate supply.
- An assessment of potential sources that could impact the water quality, located within the onshore cable route, should be undertaken and if required, appropriate mitigation should be applied.

D.7.2 Water Levels

- 23. The baseline assessment identified that natural seasonal variation will potentially result in water levels dropping below the base of proposed excavations (2m bgl) and therefore it is not proposed to stipulate trigger levels for level monitoring.
- 24. Also, it is possible for shallow wells to run dry and therefore an alternative water supply would be provided to the landowner and the following measures should be undertaken:
 - Temporarily cease dewatering to review monitoring data and determine the cause of the interruption in supply.
 - Review level monitoring and logger data to assess whether there has been a notable change in water levels since the commencement of dewatering activities.
 - If the review indicates that the dewatering is the cause then activities would cease until appropriate mitigation can be put into place.
 - If the monitoring indicates natural seasonal trends or alternate cause for loss of supply then dewatering would recommence as it was not the cause.

D.8 Enhanced Mitigation/ Control Measures

- 25. A number of pre-construction mitigation proposals are being explored by North Falls with landowners / tenant farmers, these include but are not limited to:
 - Offering a permanent mains connection to the property either in lieu of or to complement their existing supply.
 - The advancement of further well supplies either; further away from the potential dewatering activities or to a deeper depth below the cable excavation depth.
- 26. If during construction an unlikely event of an adverse impact on water quantity or quality occurs, appropriate mitigation should be put into place to provide either a temporary or permanent replacement to supply.
- 27. In the case that construction / dewatering activities causes a short term impact a temporary water supply (such as tankering / water bowser) will be provided once agreed with the PWS and the licenced abstraction owner. In the unlikely

event that the impact is assessed as longer term, a replacement well will be drilled away from the current location to remove any impact on water quality or availability of supply.







HARNESSING THE POWER OF NORTH SEA WIND

North Falls Offshore Wind Farm Limited

A joint venture company owned equally by SSE Renewables and RWE.

To contact please email contact@northfallsoffshore.com

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